

ENGLISH TRANSLATION OF THE INTERNATIONAL APPLICATION
FOR NATIONAL PHASE SUBMISSION

1

**METHOD AND DEVICE FOR ANALYZING THE COMBUSTION NOISE IN A
CYLINDER OF AN INTERNAL COMBUSTION ENGINE**

The invention is based on a method and a device for analyzing the combustion noise during the injection of fuel into a cylinder of an internal combustion engine according to the generic part of the independent claims 1 and 9. It is already known to detect the combustion noise that is caused by the pressure waves during the ignition of the fuel-air mixture in the combustion chamber with the aid of a knock sensor. However, the knock sensor detects not only the direct combustion noises, but also all further interference noises, both of the internal combustion engine itself and also in its environment.

It is further known to restrict the interference noises at least partially by activating or evaluating the noise measurement only within a fixed measuring window which is started for example after the injection of a first injection amount and terminated on completion of combustion of a following injection pulse. Although this method brings a certain improvement as regards the evaluation of the detected combustion noise, it still includes a high proportion of undesirable interference noises. Moreover, the fixed measuring window cannot be adjusted to the individual injection pulses with their different injection amounts. However, since the intensity of the combustion noise is a measure for the amount of fuel injected, the interference noises contained in the recorded combustion noise can lead to unreliable results in the evaluation. The known method is therefore to be regarded

ENGLISH TRANSLATION OF THE INTERNATIONAL APPLICATION

FOR NATIONAL PHASE SUBMISSION

2

as critical, for example, for determining an injected amount of fuel.

A further problem also resides in the fact that, in particular in the adjustment of minimal injection amounts for an internal combustion engine, each individual combustion noise of an injection pulse must be detected as accurately and reliably as possible in order to be able, for example, to precisely analyze the combustion noises between one or more pre-injections and the following main injection. Such requirements are imposed in particular on modern internal combustion engines operating with direct fuel injection such as diesel or petrol engines with piezoelectric injectors in which the injection pulses of a cycle are activated at very short time intervals.

The object underlying the invention is to specify a method and a device by means of which the combustion noise of an internal combustion engine produced during the injection of the fuel can be determined with greater accuracy and reliability. This object is achieved by means of the features of the independent claims 1 and 9.

With the inventive method or device for analyzing the combustion noise during the injection of fuel into a combustion chamber of an internal combustion engine having the features of the independent claims 1 and 9, there is produced the advantage that essentially the combustion noise of an individual injection pulse is detected. It is regarded as particularly advantageous that the smallest possible measuring window can be formed for the registering of the combustion

ENGLISH TRANSLATION OF THE INTERNATIONAL APPLICATION
FOR NATIONAL PHASE SUBMISSION

3

noise. Said measuring window is not fixed, but is variable and is adjusted to match operating conditions of the internal combustion engine. In this way it is possible, in contrast to the known methods, also to determine a small fuel amount of an individual injection pulse with improved reliability. In contrast, with known methods it can only be established roughly whether an injection or a combustion has taken place or not.

Advantageous developments and improvements of the method and device specified in the independent claims 1 and 9 are realizable by means of the measures set forth in the dependent claims. It is regarded as particularly advantageous that the end position of the measuring window is set such that it is no longer possible to record further injection and combustion noises of a following injection pulse. Since the start of a following injection pulse is determined by a control device, this moment in time or a corresponding rotation angle of the crankshaft of the internal combustion engine can easily be advantageously used to close the measuring window only in conjunction with an estimated value for the ignition delay. This moment in time is determined individually for each injection pulse and can therefore be adapted to the operating conditions of the internal combustion engine.

If the end position for the measuring window is known, it is very easy to determine a start position for the measuring window by counting back and thereby defining its length in time. In this way the measuring window can be optimally adjusted for the injection pulse or to its combustion noise.

ENGLISH TRANSLATION OF THE INTERNATIONAL APPLICATION
FOR NATIONAL PHASE SUBMISSION

4

An advantageous solution is also seen in setting the start position of the measuring window at the beginning of the injection pulse, since this time is predefined. Alternatively it is provided to place the start position at the beginning of the occurring combustion noise, which can be easily measured for example due to the increasing noise level.

A further advantageous solution for determining the start position and/or the length of the measuring window also consists in evaluating the envelope which can be formed from the combustion noise. The envelope can advantageously be formed by rectification of the received noise signals.

If the envelope is recorded over two adjacent injection pulses, then a simple evaluation with regard to a local minimum can be carried out by means of a low pass filter. The two injection pulses or their combustion noises can be easily differentiated on the basis of the local minimum. This likewise results in a simple solution for specifying the start position/end position of the measuring window.

If several local minimum values occur, the smallest minimum value is chosen for the start position, since this value provides the greatest probability for the start of the combustion noise. Thus, all interference noises that occurred previously are advantageously not recorded.

In practice it has been shown that it is of advantage if the measuring window is started at a crankshaft angle roughly in the range $\pm 4^\circ$ crk with regard to the start of the injection pulse. At the same time an ignition delay and the specific

ENGLISH TRANSLATION OF THE INTERNATIONAL APPLICATION
FOR NATIONAL PHASE SUBMISSION

5

parameters of an engine type have to be taken into account for the exact specification.

As a result of the optimized detection and evaluation of the combustion noise, the device can determine, with the aid of a comparison table for example, an actually injected amount of fuel from the intensity of the combustion noise. This can be used in particular in the case of diesel and petrol engines operating with direct fuel injection in order, inter alia, to monitor and control the actually injected amount of fuel.

An exemplary embodiment of the invention is shown in the drawing and is explained in more detail in the following description.

Figure 1 shows a schematic block diagram of the invention,

Figure 2 shows a first diagram in which the noise signals recorded by a knock sensor are depicted together with their envelope,

Figure 3 shows a second diagram of the invention including the representation of the optimized measuring window, and

Figure 4 shows a block diagram of an inventive device for detecting and evaluating combustion noises.

Figure 1 shows in a schematic representation an exemplary embodiment of a device according to the invention for analyzing the combustion noise during the injection of fuel

ENGLISH TRANSLATION OF THE INTERNATIONAL APPLICATION
FOR NATIONAL PHASE SUBMISSION

6

into a combustion chamber (cylinder) of an internal combustion engine, said embodiment being represented in the form of a block diagram. Essentially it has an algorithm which is embodied for evaluating the combustion noise detected by a knock sensor. In addition to the actual combustion noises which arise due to ignition of the air-fuel mixture in the combustion chamber or in the cylinder of the internal combustion engine, the depicted noise curve also includes further noises caused, for example, by vibrations of moving parts of the engine (pistons, crankshaft, etc.) or its auxiliary components such as generator, oil and water pump, transmission, powertrain, exhaust, etc. These interference noises overlay the actual combustion noise generated at each injection pulse. In particular diesel and petrol engines with common rail or pump-nozzle injection systems using direct fuel injection operate with finely dosed amounts of fuel which are often delivered in the form of multiple injections within one injection cycle. The control of the individual injection pulses is very complex and demands maximum precision and reliability.

In order to be able to reliably meet the requirements of operating conditions of the internal combustion engine such as emissions, consumption, smooth running, etc., it is necessary, inter alia, that a control device registers the actual amount of fuel injected during an injection pulse and then controls the injection system accordingly. Figure 1 shows the schematized sequence, which is explained below.

The signal recorded by the knock sensor is initially guided via a rectifier unit 1 in order to form an envelope for the

ENGLISH TRANSLATION OF THE INTERNATIONAL APPLICATION
FOR NATIONAL PHASE SUBMISSION

7

detected combustion noise. It is essential to the invention that the combustion signal is recorded in a measuring window that is individually adjusted for one injection pulse and can be varied according to operating conditions. The measuring window is determined with the aid of an algorithm which in particular specifies a start and an end point. The measuring window is therefore specified with regard to its position and its length relative to the rotation angle of the crankshaft. It is embodied to be as small as possible in order to register practically only the combustion noise which is associated with a selected injection pulse within one injection cycle.

For example, the end point of the measuring window is initially specified such that the measuring window is closed prior to the start of the combustion noise of a following injection pulse. The start point of the measuring window can easily be counted back for a predefined fixed length of the window. By this means the components of the combustion noise before and after the start of the injection pulse (SOI) are recorded.

In a further embodiment of the invention it is provided to place the start point of the measuring window at the start of the combustion noise. This point can be recognized for example by a rise in the envelope curve.

Alternatively it is provided to place the measuring window in such a way that it is active only during the occurrence of the combustion noise and is activated at the start of the combustion noise.

ENGLISH TRANSLATION OF THE INTERNATIONAL APPLICATION
FOR NATIONAL PHASE SUBMISSION

8

The envelope of the combustion noise obtained from the rectification is subsequently routed to a low pass filter 2. This part of the algorithm determines one or more local minimum values for example by differentiating or filtering the envelope. A local minimum value typically occurs between two injection pulses, for example between a pre-injection and a main injection. It thus localizes the start of the combustion noise.

If a number of local minimum values occur, the smallest local minimum value is filtered out, for example by comparison of the found local minimum values, in a minimum determination unit 3. This absolute local minimum value is then specified for the start of the combustion noise and can then be tapped at the output of the unit 3 for the start point of the measuring window.

It has been shown that the start point of the measuring window relative to the start of injection (SOI) can be changed by a crankshaft angle $\pm 4^\circ$ crk. In this case an ignition offset of approx. -6° crk also has to be taken into account in the main injection for a corresponding engine type.

As already mentioned, the length of the measuring window can also be varied. If the start point of the measuring window has been determined by analysis of the envelope, a variable window length can be chosen. However, this requires a compensation factor by means of which different, length-dependent signal energies can be made comparable.

ENGLISH TRANSLATION OF THE INTERNATIONAL APPLICATION
FOR NATIONAL PHASE SUBMISSION

9

The modules 2 and 3 are preferably implemented by means of a software program which is processed by a corresponding device.

The waveform of the unfiltered noise signal G (structure-borne sound signal) recorded by a knock sensor is shown in the first diagram according to Figure 2. The scaling on the y-axis indicates the amplitude and hence the noise intensity. The rotation angle of the crankshaft in °crk has been plotted on the x-axis. The curve shown in bold corresponds to the envelope H which was obtained by the rectification.

As can be seen from the diagram, the amplitudes of the noise signal G are particularly strong in the middle range, whereas they run more weakly to the right and left thereof. The middle range of this noise signal G corresponds to that of an injection pulse, for example a main injection, while the waveform at the sides corresponds to the interference signal. The envelope H has a similar shape. Its amplitude is considerably smaller at the edge sides than in the range of the injection pulse. It is also striking that the envelope H has two local minimum values M1, M2 in the middle range, with M2 forming the smallest local minimum value. The two local minimum values can be determined by means of the low pass filter or by derivation of the envelope according to Figure 1. The smallest local minimum value M2 is thus used as the start of combustion noise (SOC).

Figure 3 shows a second diagram in which the noise signals G are again represented as an oscillating curve. The determined measuring window M has also been entered in addition to this curve. As can be seen from Figure 3, the measuring window M is

ENGLISH TRANSLATION OF THE INTERNATIONAL APPLICATION
FOR NATIONAL PHASE SUBMISSION

10

activated roughly in the range 175 to 190° crk, while all other ranges are suppressed. This range corresponds to the combustion noise of an individual injection pulse of the second cylinder of the internal combustion engine. On the other hand, further injection pulses, as shown somewhat further to the right of the measuring window M in Figure 3, are suppressed and so cannot influence the evaluation of the combustion noise that is to be considered.

In order to be able to determine the actually injected amount of fuel from the amplitude or the intensity of the combustion noise measured within the measuring window M, reference is made to a comparison table which was previously determined for a specific engine type, specific operating parameters, a specific length of the measuring window M, etc.

Figure 4 shows a device for analyzing the combustion noise which is represented schematically as a block diagram. A control device 15 is preferably connected via a bus system to a knock sensor 14 which is generally embodied as a structure-borne sound sensor. The knock sensor 14 is arranged at a suitable position of the internal combustion engine 10, ideally in proximity to the cylinder 11. The internal combustion engine 10 has typical modules: at least one cylinder 11 in which a piston 12 is arranged in an alternately movable manner and which transfers its kinetic energy via a connecting rod to a crankshaft 18. An injection valve or injector 13 is mounted at a suitable position for the purpose of injecting fuel into the combustion chamber of the cylinder 11. The injector 13 is preferably actuated by a

ENGLISH TRANSLATION OF THE INTERNATIONAL APPLICATION
FOR NATIONAL PHASE SUBMISSION

11

piezoelectric actuator. In this arrangement the fuel flows under high pressure via a feed line 13a into the injector 13.

For the purpose of determining the rotation angle crk of the crankshaft 18, an angle sensor 17 is preferably arranged at a toothed flywheel ring of the crankshaft 18 so that the current rotation angle of the crankshaft 18 can always be precisely determined. The signals of the angle sensor 17 are likewise transferred via the bus system to the control device 15.

The control device 15 has the usual units, such as a program-controlled computer, a memory 16, evaluation units, etc. These units have already been explained in the foregoing. The software program with the algorithm according to the invention, along with the captured or determined data, comparison tables, etc., is stored at least temporarily in the memory 16 for as long as they are needed for the data processing or for control of the internal combustion engine 10.